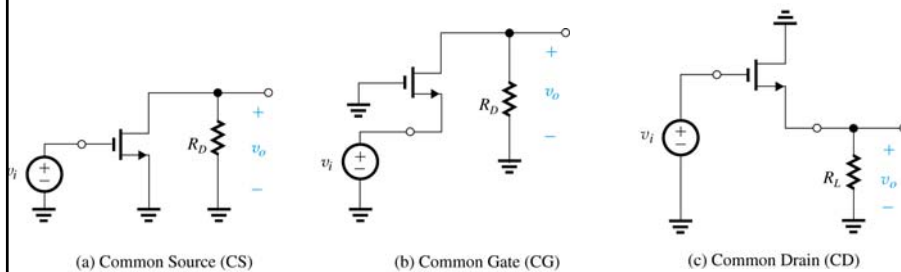


MOSFET Amplifier Configuration

- Single stage
- The signal is fed to the amplifier represented as v_{sig} with an internal resistance R_{sig} .
- MOSFET is represented by its small signal model.
- Generally interested of gain, input and output resistance (overall amplifier circuit not only the small signal model).

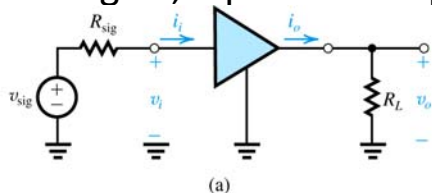
MOSFET Amplifier Configuration

- Considering only the small signal not the bias



Characterizing Amplifiers

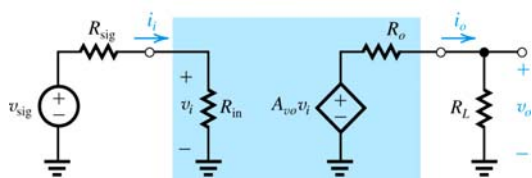
- Find gain, input and output resistance



(a)

$$R_{in} = \frac{v_i}{i_i}$$

$$A_{VO} = \left. \frac{v_o}{v_i} \right|_{R_L = \infty}, A_V = \frac{v_o}{v_i}$$



(b)

$$G_v = \frac{v_o}{v_{sig}} \text{ Overall voltage gain}$$

Amplifier Configuration

- Common Source
- Common Source with a source resistance
- Common gate
- Common drain or voltage follower

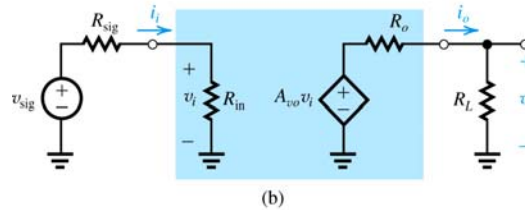
Amplifiers

$$v_o = A_{vo} v_i \frac{R_L}{R_L + R_o}$$

$$v_i = v_{sig} \frac{R_{in}}{R_{in} + R_{sig}}$$

$$A_v = A_{vo} \frac{R_L}{R_L + R_o}$$

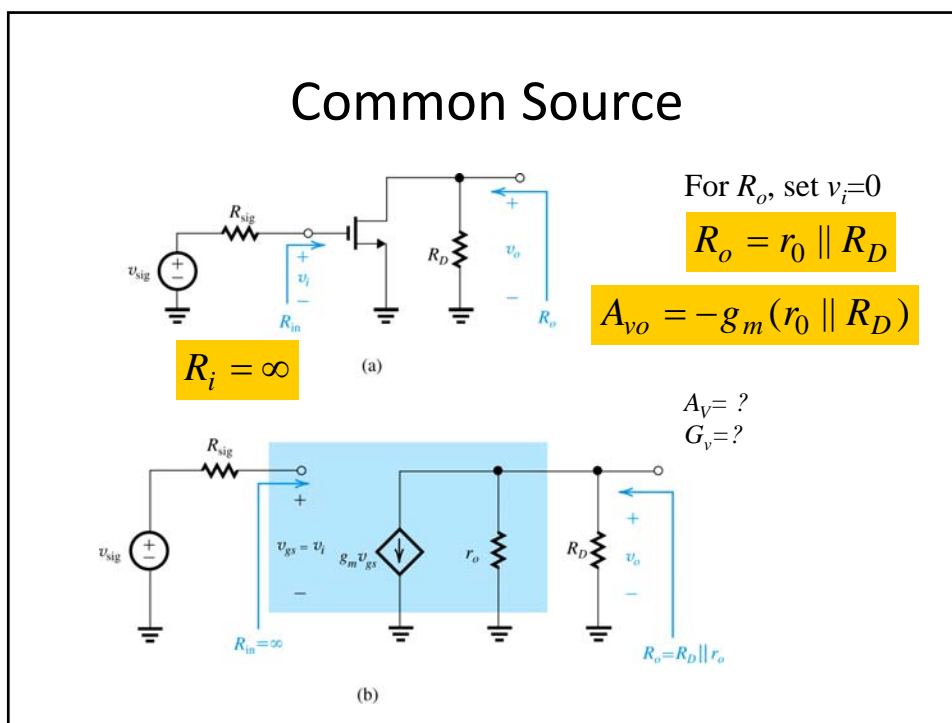
$$G_v = \frac{v_o}{v_{sig}} = \frac{R_{in}}{R_{in} + R_{sig}} A_{vo} \frac{R_L}{R_L + R_o}$$



Common Source

- Most widely used configuration
- In multistage amplifiers, the bulk of the gain is from common source.
- The source is grounded, making it common between input and output.
- We can use hybrid π model.

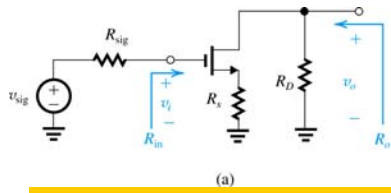
Common Source



Common Source with Source R

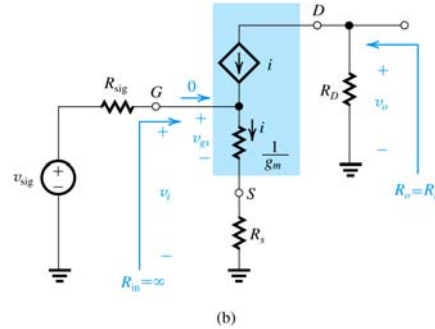
- For simplicity, r_o is not included.
- No effect on discrete implementation, not so for IC's
- R_s provides a negative feedback to control the magnitude of the signal to prevent nonlinear distortion.
- Also reduces the voltage gain and extends the useful bandwidth.

Common Source with Source R

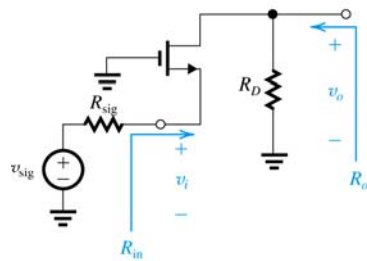


$$v_{gs} = -g_m v_i \frac{1/g_m}{1/g_m + R_S}$$

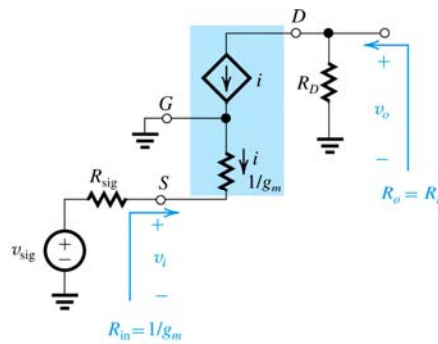
$$v_{gs} = \frac{v_i}{1 + g_m R_S}$$



Common Gate Amplifier

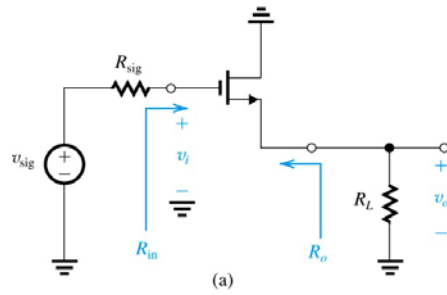


(a)



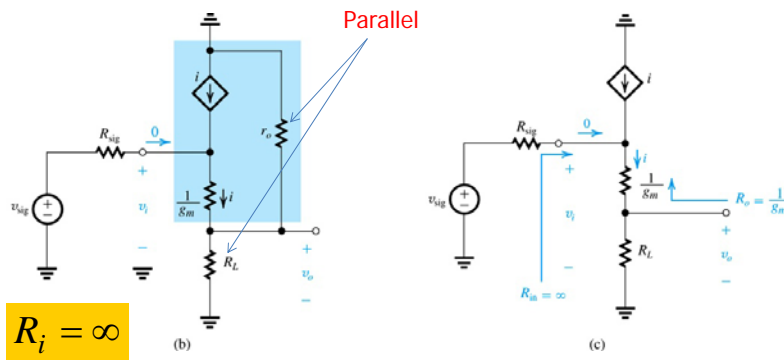
(b)

Common Drain Amplifier – Source Follower



Since there is a resistance R_L connected to the source, it is easier to use the T-model

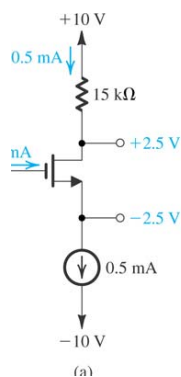
Common Source – Voltage Follower



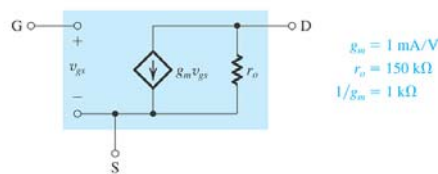
Comparison

	CS	CS+RS	CG	CD
Rin	∞	∞	$\frac{1}{g_m}$	∞
Rout	$R_D \parallel r_o$	R_D	R_D	$1/g_m$
G	$-g_m(R_D \parallel R_L \parallel r_o)$	$A_v = \frac{g_m(R_D \parallel R_L)}{1 + g_m R_S}$	$G_v = \frac{(R_D \parallel R_L)}{1/g_m + R_{sis}}$	$G_v = \frac{A_v R_L}{1/g_m + R_L}$

Example E5.37



$V_{OV} = 1V$
 $V_{GS} = 2.5V$

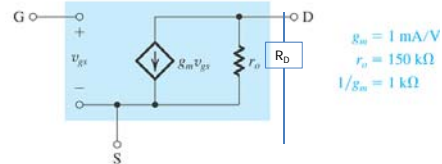


$V_{DD} = V_{SS} = 10V, I = 0.5mA, R_G = 4.7M\Omega, R_D = 15K\Omega,$
 $V_t = 1.5V, k_n = 1mA/V^2, V_A = 75V$

Find $V_{OV}, V_{GS}, V_G, V_S, V_D, g_m, r_o$
 What is the max. possible voltage swing at drain and the MOSFET remains in saturation?

Example 5.38

Find R_{in} , A_{vov} , R_o , G_v with and without r_o . $R_{sig} = 100\text{K}\Omega$ and $R_L = 15\text{K}\Omega$

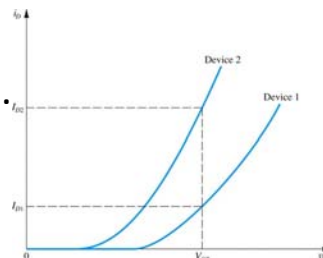


Biassing in MOS Amplifiers

- How to choose the operating point?
- Want a stable Q-point (known I_D and V_{DS}) to ensure operation in the saturation region.

Biasing -- Fixing V_{GS}

- I_D depends on μ , C_{ox} , W/L and V_p , and V_{GS}
- C_{ox} , V_{GS} (even W/L) can vary across devices of the same type.
- Constant V_{GS} Not a good idea .
- μ, C_{ox} are a $f(t)$



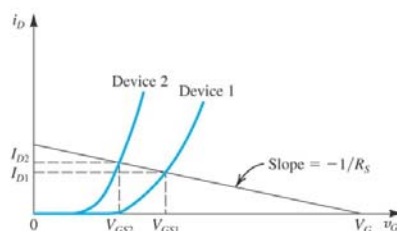
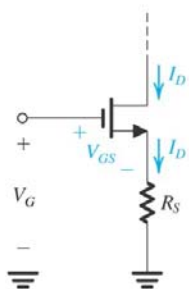
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Biasing – Fixing V_G and R_S

- R_S provides a negative feedback to stabilize I_D



Biassing – Fixing V_G and R_S

- Uses one power supply
- What is the effect on input resistance when you add v_{gs} signal

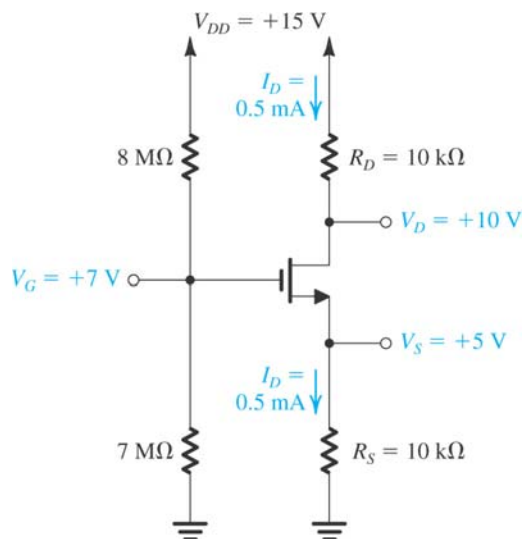
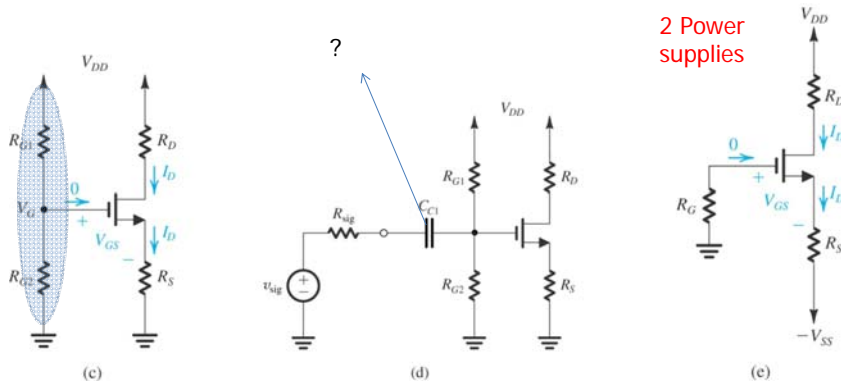
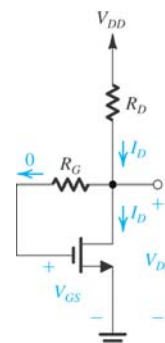


Figure 5.53 Circuit for Example 5.12.

Biassing – D-to-G Resistor

- $V_{GS} = V_{DS} = V_{DD} - I_D R_D$
- $V_{DD} = V_{GS} + I_D R_D$
- Provides a feedback resistor to stabilize I_D

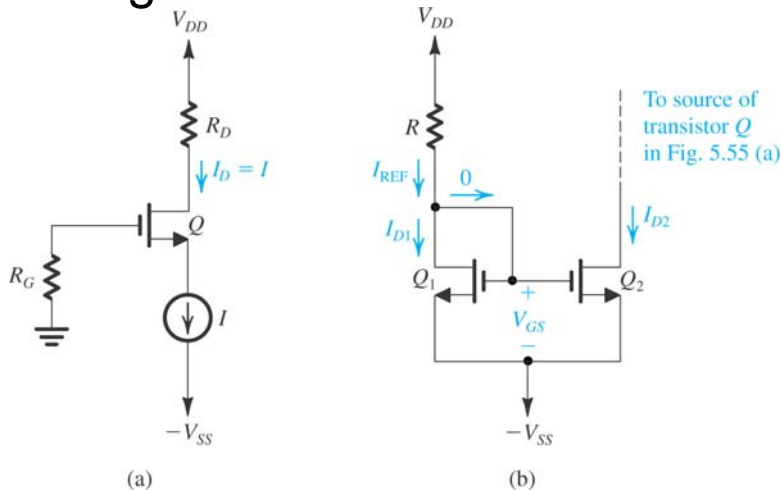


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Biassing – Constant Current Source

Figure 5.55 (a) Biasing the MOSFET using a constant-current source I . (b) Implementation of the constant-current source I using a current mirror.

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Frequency Response

