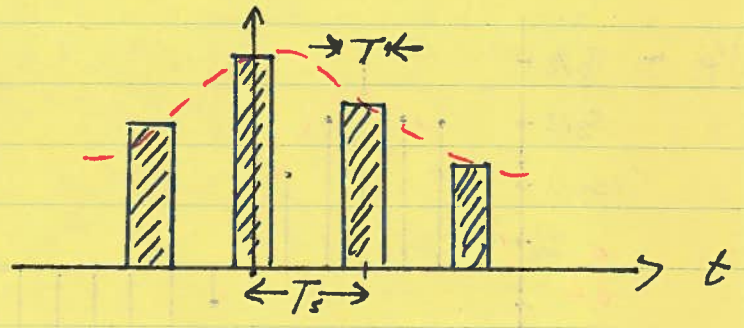


# 2.6 Quantization & Encoding

## 6.1 Pulse Amplitude Modulation

- the process of (or result) of flat top sampling can more generally be viewed as a transformation of your signal...  
... into a series of pulses with varying amplitude



- people generally refer to this as PAM and it appears in other (although fundamentally identical) contexts

- in general modulation is when you multiply your signal by some other periodic waveform typically referred to as the carrier

- are we justified in calling this sampling modulation?

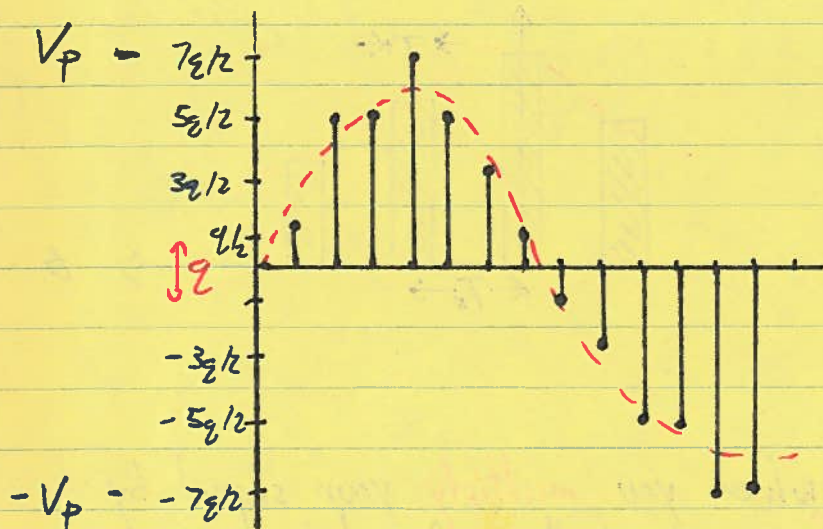
$$\begin{aligned}
 \text{recall } x_s(t) &= [x(t) \chi_s(t)] * p(t) \\
 &= \left[ \sum_{n=-\infty}^{\infty} x(nT_s) \delta(t - nT_s) \right] * p(t) \\
 &= \sum_{n=-\infty}^{\infty} x(nT_s) p(t) * \delta(t - nT_s) \\
 &= \sum_{n=-\infty}^{\infty} x(nT_s) p(t - nT_s)
 \end{aligned}$$

commutative  
 $\chi_1 * \chi_2 = \chi_2 * \chi_1$   
 $\int_{-\infty}^{\infty} x(t) \delta(t - t_0) dt = x(t - t_0)$

- thus we are multiplying our signal by a periodic pulse train...  
... a carrier... we are modulating  $\rightarrow$  PAM

# 6.2 Quantizing

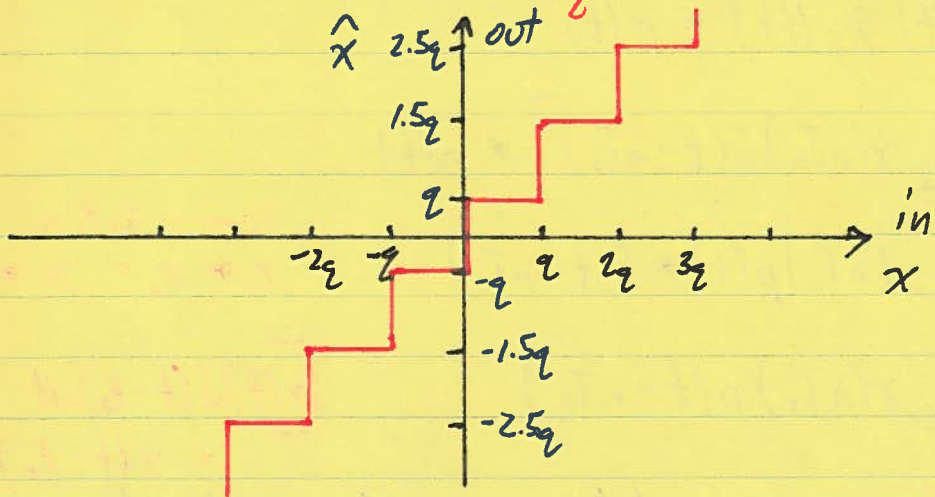
- Our **sampling/PAM** has resulted in **discrete-time** signals but with **continuous amplitude range**
- If you want to **digitize** this ... you have to **approximate** with one of a number of **discrete levels**



- say you choose a range from  $-V_p$  to  $+V_p$
- if you divide this into  $L$  **equally spaced levels** centred at zero
- the **quantile interval** (separation between levels) is

$$q = \frac{2V_p}{L-1} = \frac{V_{pp}}{L-1} = \frac{V_{pp}}{2^b-1} \approx \frac{V_{pp}}{2^b}$$

- we can sketch the **quantizer** as a **transfer function**

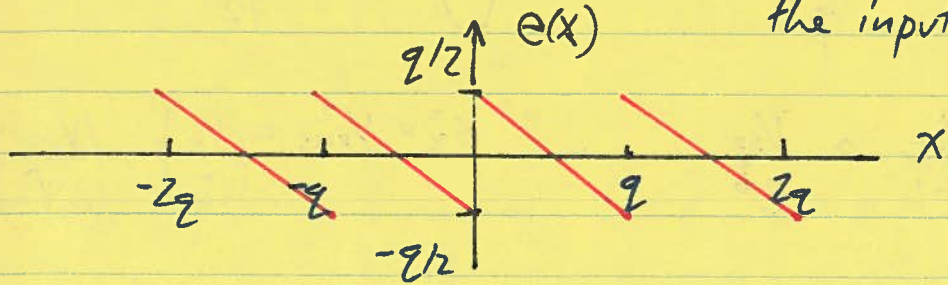




### 6.3 Quantization Error

$$\hat{x}(t) = x(t) + e(t)$$

an error dependent on the input signal and  $q$



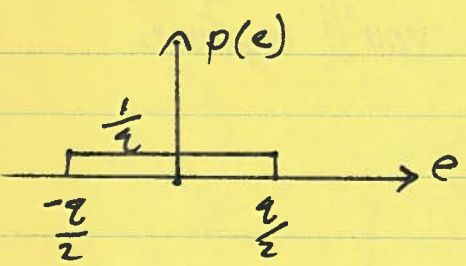
- mean square value (variance) of this error is a useful quantification

$$e(x) = -x + \frac{q}{2} \quad e^2 = x^2 - xq + \frac{q^2}{4}$$

$$\langle e^2 \rangle = \sigma_q^2 = \frac{1}{q} \int_0^q (x^2 - xq + \frac{q^2}{4}) dx = \frac{1}{q} \left[ \frac{x^3}{3} - \frac{qx^2}{2} + \frac{q^2 x}{4} \right]$$

↑ periodic w/  $q$   
 assume uniform dist  
 (i.e.  $p(x) = 1/q$ )

$$= \frac{q^2}{2} \left[ \frac{4-6+3}{12} \right] = \frac{q^2}{12} \dots \text{none formally} \dots \checkmark$$



$$\sigma_q^2 = \int_{-q/2}^{+q/2} e^2 p(e) de = \int_{-q/2}^{q/2} \frac{e^2}{q} de = \frac{e^3}{q \cdot 3} \Big|_{-q/2}^{q/2}$$

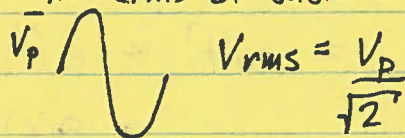
$$= \frac{1}{q} \left[ \frac{q^3}{3 \cdot 8} - \frac{-q^3}{3 \cdot 8} \right] = \frac{q^2}{12} = \sigma_q^2$$

In general SNR is then

$$SNR = \frac{\sigma_x^2}{\sigma_q^2} = \sigma_x^2 \cdot \frac{12}{q^2}$$

FULL POWER SIGNALS:

in terms of basic sin wave case



$$V_{rms} = \frac{V_p}{\sqrt{2}}$$

recall  $q = \frac{V_{pp}}{L-1} \approx \frac{V_{pp}}{2^b}$

$$\sigma_x^2 = V_{rms}^2 = \left(\frac{V_p}{\sqrt{2}}\right)^2 = \left(\frac{V_{pp}}{2\sqrt{2}}\right)^2 = \frac{V_{pp}^2}{8}$$

$$\therefore SNR = \sigma_x^2 \times 12 \times \frac{2^{2b}}{V_{pp}^2}$$

$$SNR_{dB} = \left[ \log(2^{2b}) + \log 12 + \log\left(\frac{\sigma_x^2}{V_{pp}^2}\right) \right] \times 10$$

$$= 6.02b + 10.8 + 10 \log\left(\frac{\sigma_x^2}{V_{pp}^2}\right)$$

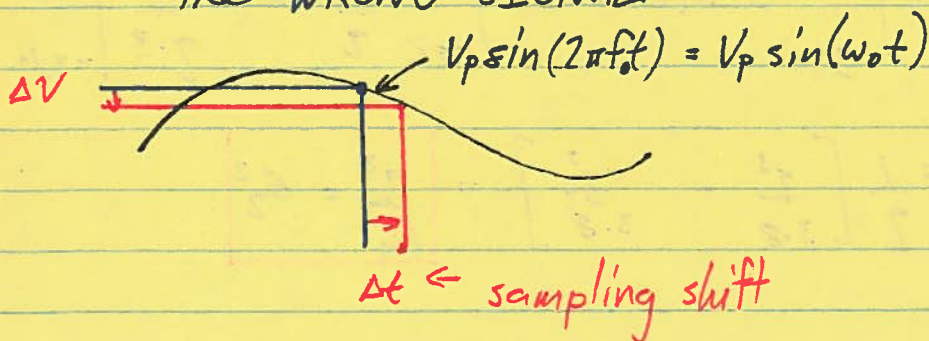
$$= 6.02b + 1.77 \text{ if } \sigma_x^2 \text{ is FULL POWER}$$

-OR-

$$SNR = \frac{V_{pp}^2}{8} \times \frac{12}{q^2} = \frac{V_{pp}^2}{8} \times \frac{12}{\frac{V_{pp}^2}{2^{2b}}} = \frac{3}{2} \times 2^{2b} = \frac{3}{2} (L-1)^2$$

### 6.4 Timing Jitter

if your sampling clock moves around you'll capture the WRONG SIGNAL





$\sigma_j^2 = E\{\Delta v^2\}$  ... clearly signal slope is influential so...

$$= E\left\{\left(\frac{dv}{dt}\right)^2 \cdot \Delta t^2\right\}$$

$$= E\left\{\left(\frac{dv}{dt}\right)^2\right\} \cdot E\{\Delta t^2\}$$

$$= E\left\{(V_p \times 2\pi f_0 \times \cos(2\pi f_0 t))^2\right\} \cdot \sigma_t^2$$

$$= \frac{V_p^2 \omega_0^2}{2} \cdot \sigma_t^2$$

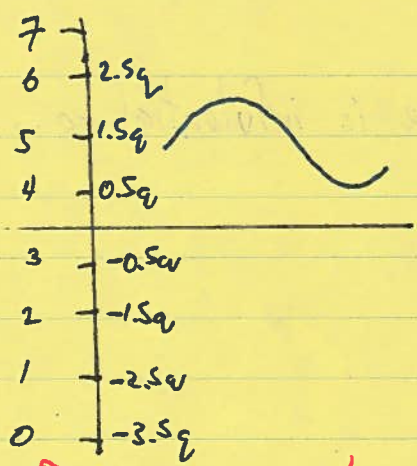
$$\therefore SNR = \frac{\sigma_x^2}{\sigma_j^2} = \frac{V_p^2}{2} / \frac{V_p^2 \omega_0^2 \sigma_t^2}{2} = \frac{1}{\omega_0^2 \sigma_t^2} = \frac{1}{4\pi^2 f_0^2 \sigma_t^2}$$

• more generally for a signal from  $f_L$  to  $f_H$  you can show

$$SNR = \frac{1}{\sigma_t^2} \times \frac{3}{(f_H^2 + f_H f_L + f_L^2)} \approx \frac{3}{\sigma_t^2 \cdot f_H^2}$$

### 6.5 Encoding

- Our quantizer produces a discrete set of voltage levels
- The job of the encoder is to convert this into a suitable digital code number

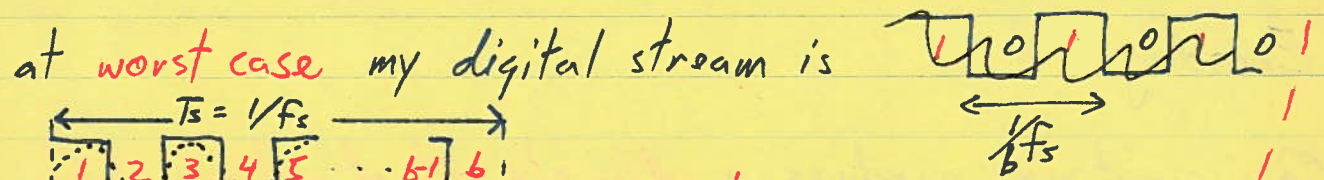


- this mapping onto some code is, in general, called **PCM**
- PCM **code number** is of course represented as a **binary sequence**
- basically PCM encodes each level into a **digital word**

- what are PCM's **bandwidth requirements** ???
- If I use **L** levels ∴ need

$$b = \log_2 L \text{ bits}$$

- if **message BW** is  $f_m$  and **sampling rate** is  $f_s \geq 2f_m$
- ∴  $b f_s$  **bits rate** is needed ← **data bandwidth**
- but what's ~~is~~ my **signal bandwidth** ?



$\frac{T_s}{b/2} \Rightarrow$  ∴ our highest <sup>harmonic</sup> freq. component is  $\frac{b f_s}{2}$

∴ our PCM signal's bw  $f_{PCM} = \frac{b f_s}{2} \geq b f_m$

→ clearly steps must be taken to compress this